

Vertically Ordered Hematite Nanotube Array as an Ultrasensitive and Rapid Response Acetone Sensor

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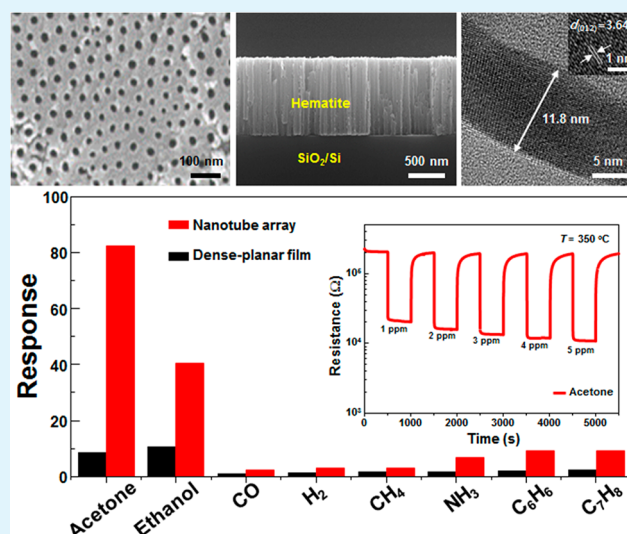
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S Supporting Information

ABSTRACT: Vertically ordered nanotube array is a desirable configuration to improve gas sensing properties of the hematite which is the most abundant and cheapest metal oxide semiconductor on earth but has low and sluggish chemiresistive responses. We have synthesized a vertically aligned, highly ordered hematite nanotube array directly on a patterned SiO₂/Si substrate and then it used as a gas sensor without additional processing. The nanotube array sensor shows unprecedentedly ultrahigh and selective responses to acetone with detection limits down to a few parts per billion and response time shorter than 3 s.



KEYWORDS: hematite, nanotube array, acetone sensor, earth abundant, ultrasensitive

Semiconducting metal oxide gas sensors have considerable interests in diverse applications such as environmental monitoring, agriculture, medical diagnosis, aerospace industries, and mobile applications because of their small size, low cost, and simplicity in operation.^{1,2} Various oxide materials including SnO₂, WO₃, ZnO₂, and TiO₂, have so far been studied. Beside them, hematite (α -Fe₂O₃), one of the most stable iron oxide forms, has been identified as a promising candidate as a gas sensing material since it is a chemically stable n-type semiconductor with the band gap energy of 2.2 eV. More importantly, hematite is the most abundant and cheapest semiconductor metal oxide which we can obtain on earth. According to the U.S. Geological Institute, the world mineral resources of iron are estimated to exceed 800 billion tonnes (Figure 1a).³ The annual world production of iron was reported up to 3.1 billion tonnes in 2012 (Figure 1b). This value is approximately 4 orders of magnitude higher than the annual production of Sn from which the oxide SnO₂ is most widely used for gas sensors. Nevertheless, gas sensors based on

hematite have been rarely explored for the detection of a variety of gases due to their low sensitivities and sluggish response compared with gas sensors based on SnO₂.^{4,5}

It is well-known that nanostructure possesses high surface-to-volume ratio, increased surface activity, and strong adsorption/desorption ratio of the target gas molecules, so the metal oxide nanostructures are expected to excellent gas sensing performance.^{6,7} For instance, gas sensors based on one-dimensional metal oxide nanostructures such as nanowires, nanorods, nanobelts, and nanotubes, have been widely exploited for gas sensor application. However, low-cost and high yield mass production of one-dimensional metal oxide materials as gas sensors remains still challenging. Vertically ordered nanotubes prepared by facile anodic oxidation of metal are considered as a promising configuration for gas sensors. Particularly, extremely

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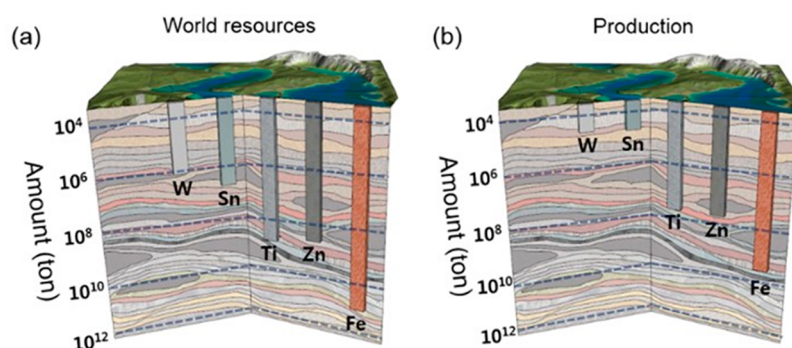


Figure 1. (a) World mineral resources on earth and (b) world production on 2012 for W, Sn, Ti, Zn, and Fe. Data for the plots were extracted from Mineral Commodity Summaries 2013 provided by U.S. Geological Survey.³

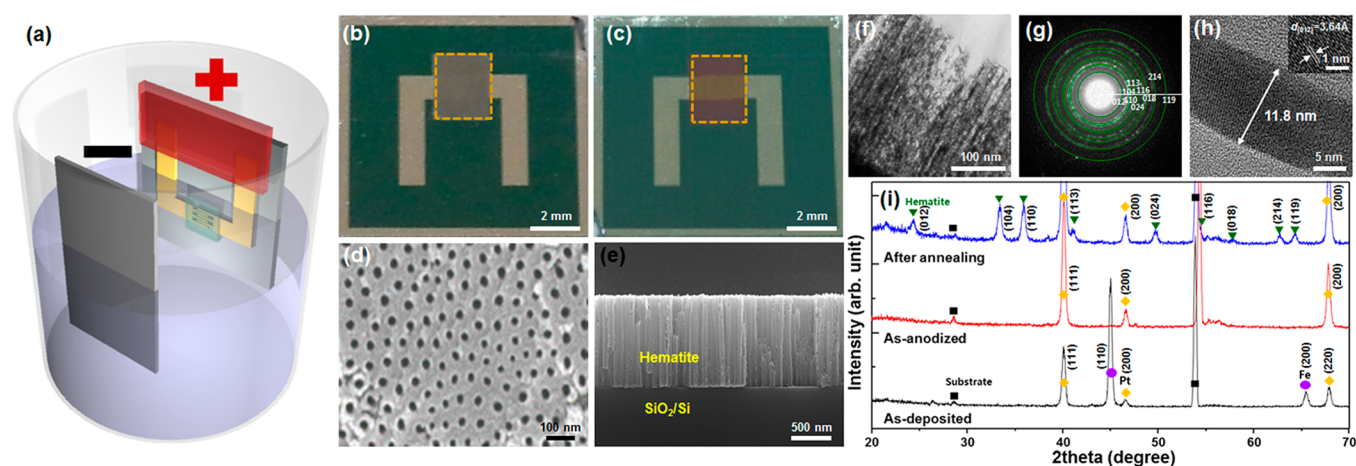


Figure 2. (a) Sketch illustrating our anodization method to form Fe_2O_3 nanotube array on Pt-IDEs-patterned SiO_2/Si substrate. The key idea of our method is clamping the Pt electrodes as the current spreader during anodization. (b, c) Photographs of a Fe film on Pt-patterned SiO_2/Si substrate (b) before anodization and (c) after anodization. (d) Plain-view SEM images of Fe_2O_3 nanotube array on Pt-IDEs-patterned SiO_2/Si substrate. (e) High magnification cross-sectional SEM images of the Fe_2O_3 nanotube array. (f) Cross-sectional TEM image of hematite nanotube array. (g) Selected area diffraction pattern with indexing. (h) High-magnification TEM image of the wall thickness of a hematite nanotube. The inset shows the interplanar spacing of 0.364 nm corresponding to a (012) plane. (i) Glancing angle X-ray diffraction patterns of a Fe/Pt/ SiO_2/Si structure before anodization and Fe_2O_3 nanotube arrays before and after annealing at 550 °C for 5 h.

large specific surface area compared with dense planar film counterparts provides excellent adsorption and desorption of gas molecules, which is desirable for high-performance gas sensors.

To date, the synthesis of hematite nanotubes has relied on hydrothermal,⁸ template-assisted,⁹ and electrochemical anodization methods.¹⁰ Hydrothermal synthesis is a simple method to prepare nanotubular structures, but typically involves harsh chemical conditions such as low or high pH which leads to substrate damage. In addition, because the synthesized hematite nanotubes are composed of randomly distributed, the intrinsic large surface area of hematite nanotubes cannot be fully utilized for gas sensing. Template-assisted method using anodic aluminum oxide (AAO) has been a simple synthetic route to prepare nanotubular structures. However, the AAO templating is not compatible with high throughput semiconductor fabrication processes. The anodization of Fe foils can lead to hematite nanotubes. However, the anodization of Fe foils has not been exploited for chemiresistive gas sensors since the remained Fe foils beneath the nanotubes easily form electrical shorts with the sensor electrodes. In addition, the concurrent oxidation of the underlying Fe foils at elevated temperatures hinders reliable gas sensing performance. Alternatively, the most attractive approach is the direct synthesis of vertically

ordered hematite nanotubes on patterned SiO_2/Si substrates through electrochemical anodization. However, no work has been reported on the synthesis of hematite nanotubes on a foreign substrate because there are some difficult problems to be solved. Usually, the quality of metal oxide nanotube array obtained by the anodization of a metal film on a foreign substrate is worse than that by the anodization of a free-standing metal foil.^{11–13} The clamped area for electrical contact remains unanodized. In addition, the complete anodization of Fe into Fe_2O_3 is hard to be achieved owing to the occurrence of potential gradients in the Fe film during anodization. The key idea of our anodization method to achieve the complete anodization of the whole area of Fe film into Fe_2O_3 nanotube array is the use of Pt bottom electrodes as the current spreader for anodization. This strategy has not been applied to the synthesis of a hematite nanotube array.

Recently, selective acetone sensing attracts interests for the application in the diagnosis of diabetes from human exhaled breath.¹⁴ For semiconducting metal oxide gas sensors, selective acetone sensing against interfering gases such as ethanol and toluene have been achieved mainly using the optimization of the operating temperatures.¹⁵ Here, we report that a vertically ordered hematite nanotube array on a patterned SiO_2/Si substrate can be utilized as a selective acetone sensor. The

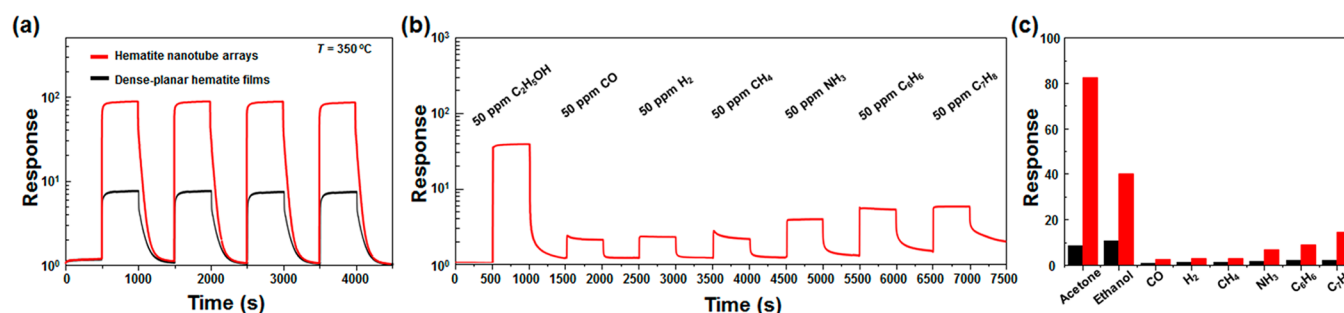


Figure 3. (a) Dynamic sensing transients of the dense-planar hematite films and hematite nanotube array to 50 ppm acetone at 350 °C. (b) Sensing transients of the hematite nanotube array to various gases. (c) Response of dense-planar hematite films and the hematite nanotube array to various gases.

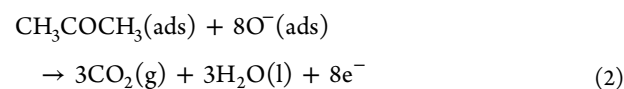
direct synthesis of a hematite nanotube array on SiO₂/Si substrates patterned with Pt electrodes leads to ultrasensitive and selective sensors to acetone. In addition, the 90% response time of the hematite nanotube sensor is ~3 s, which is much shorter than that of the dense-planar hematite film, suggesting the potential use of the hematite nanotube sensor for the noninvasive diagnosis of human diabetes.

Figure 2a shows a sketch illustrating our anodization method to form a hematite nanotube array with Pt IDEs used in this study. The details of the experimental methods are described in the Supporting Information. The key idea of our method to accomplish the complete anodization of the whole area of the Fe film into Fe₂O₃ nanotube array is clamping the Pt IDEs rather than the Fe film itself for the anodization. By clamping the Pt IDEs which cannot be anodized, the current efficiently spreads through the underlying Pt IDEs to the Fe film, potential gradients do not establish within the Fe film, resulting in the uniform anodization of Fe to Fe₂O₃. In particular, when the thickness of the remaining Fe film is very thin, the current flow through Pt IDEs to the Fe film is still effective, leading to the complete anodization of the Fe film without unconverted regions. We found that the quality of the initial Fe film is critical for the formation of vertically ordered nanotube array. When the Fe film was deposited at 400 °C, the film was observed to be highly textured with columnar grains (see the Supporting Information, Figure S1). Vertically ordered Fe₂O₃ nanotube array could be obtained from the anodization of the Fe film deposited at 400 °C. The photographs in Figure 2b, c show that the Fe film was converted to semitransparent reddish Fe₂O₃ after anodization. The plain-view SEM image in Figure 2d shows the Fe₂O₃ nanotube array formed on a Pt-IDE-patterned SiO₂/Si substrate. By cross-sectional SEM, we have confirmed that the Fe film was completely converted to Fe₂O₃ nanotube array by SEM. The synthesized Fe₂O₃ nanotube array was vertical and unprecedentedly highly ordered with uniform diameters of ~70 nm as shown in Figure 2e. This result indicates that vertically ordered Fe₂O₃ nanotube array could be directly synthesized on SiO₂/Si substrate using the present anodization method. To the best of our knowledge, no previous studies have been published for direct synthesis of a highly ordered hematite nanotube array on a foreign substrate.

The TEM image in Figure 2f shows that the nanotube array is vertically ordered with uniform diameters. The selected area electron diffraction (SAED) pattern (Figure 2g) confirms again the polycrystalline characteristics of the Fe₂O₃ nanotube array after annealing at 550 °C. The SAED pattern could be indexed as the pure hematite phase of Fe₂O₃ with lattice constants of $a = 5.0345 \text{ \AA}$, and $c = 13.7524 \text{ \AA}$ (JCPDS#87-1164). The high-

resolution TEM image (Figure 2h) reveals that a hematite nanotube array is faceted with a (012) plane with the interplanar spacing of 0.364 nm. It reveals that the wall thickness is ~12 nm, indicating that the inner diameter of the nanotube is about 50 nm. The XRD patterns of a Fe film and Fe₂O₃ nanotube array before and after annealing at 550 °C are presented in Figure 2i. No metallic Fe peak was observed from the as-anodized nanotube array, which confirms the complete conversion of the Fe film to Fe₂O₃ nanotube array. Because the as-anodized Fe₂O₃ nanotube array is amorphous, no diffraction peaks are observed. After annealing, the Fe₂O₃ nanotube array showed sharp peaks corresponding to the hematite phase without secondary phases.

A typical response curve of the hematite nanotube array to 50 ppm acetone at 350 °C is shown in Figure 3a. The response, S , is defined as $R_{\text{ambient}}/R_{\text{gas}}$ for the reducing gases (acetone, ethanol, CO, H₂, C₆H₆, C₇H₈, NH₃, and CH₄) where R_{gas} and R_{ambient} denote resistances in the presence and the absence of a test gases, respectively. Upon exposure to acetone, the hematite nanotube array quickly responded with a decrease in resistance, which revealed the typical n-type semiconducting behavior of the hematite nanotube array. Compared with the reference sensor based on a dense-planar hematite film (see the Supporting Information, Figure S2), the hematite nanotube array exhibits about 10 times higher responses to 50 ppm acetone. The gas sensing mechanism of the hematite nanotube array can be explained by the surface-depletion model.¹⁶ When the hematite nanotube array is exposed to dry air, oxygen ions are adsorbed onto the hematite nanotube surface. Therefore, the depletion layer may extend throughout the whole area of the hematite nanotube array, which leads to high resistance. On the other hands, upon exposure to reducing gas such as acetone, gas molecules will react with the chemisorbed oxygen ions at the hematite nanotube surface to form CO₂ and H₂O (as shown in eqs 1 and 2). This increases the charge carrier concentration in the hematite nanotube walls and narrows the surface depletion layer width, which leads to decrease in the resistance of the hematite nanotube array (see the Supporting Information, Figure S3).



The maximum response of acetone is as high as 84, which is much higher those of previously reported for high sensitivity sensors based on hematite nanotubes, porous hematite,

Table 1. Gas Responses of Different Hematite Nanostructures to Various Gases, As Reported in the Literature and the Present Study

sensing materials	method	conc. (ppm)	S_{acetone}	S_{ethanol}	S_{ammonia}	S_{CO}	S_{benzene}	S_{toluene}	S_{hydrogen}	S_{methane}	$T_{\text{sens}} (^{\circ}\text{C})$	ref
$\alpha\text{-Fe}_2\text{O}_3$ NTs	anodization	50	84	40.2	9.5	4.2	10.7	18.6	5.1	5.6	350	in this study
$\alpha\text{-Fe}_2\text{O}_3$ NTs	AAO templating method	50		27					2.25		RT	9
$\alpha\text{-Fe}_2\text{O}_3$ NTs	hydrothermal	20	15	7	2.5						270	17
		2000	110	42	17							17
Pt-doped $\alpha\text{-Fe}_2\text{O}_3$ spheres	solvothermal	100		2.55							400	18
porous $\alpha\text{-Fe}_2\text{O}_3$	hydrothermal	1000	92	124								19
porous $\alpha\text{-Fe}_2\text{O}_3$ spheres	hydrothermal	50		6.8							260	20
spherulike $\alpha\text{-Fe}_2\text{O}_3$ nanocrystal	solvothermal	400		79.7								21
$\alpha\text{-Fe}_2\text{O}_3$ nanoparticles	solid-stat chemical reaction	100	22.4	21.1							270, 255	22
Sn-doped wheat sheaflike $\alpha\text{-Fe}_2\text{O}_3$	hydrothermal	100		8.8							250	23
hollow $\alpha\text{-Fe}_2\text{O}_3$ polyhedras	hydrothermal	500		42.5							270	24
porous Au/ $\alpha\text{-Fe}_2\text{O}_3$	hydrothermal	500	78.3								300	25
urchinlike $\alpha\text{-Fe}_2\text{O}_3$	hydrothermal	100	10	12							260, 275	26
X-shaped $\alpha\text{-Fe}_2\text{O}_3$ crystal	hydrothermal	250				1.85	1.95				300	27
urchinlike Ag/ $\alpha\text{-Fe}_2\text{O}_3$ spheres	hydrothermal	200	75.1	55.2							350	28
$\alpha\text{-Fe}_2\text{O}_3$ hollow spheres	hydrolysis process	100		27		1.7	5				300	29
bundlelike $\alpha\text{-Fe}_2\text{O}_3$ nanorods	hydrothermal	100	38.5	26.8				7.8			250	30

hematite spheres, nanocrystals, nanoparticles, and nanorods (Table 1).^{9,17–30} This exceptional response of the hematite nanotube array is attributed to the porous nanostructure with high surface-to-volume ratio. To identify the selectivity of the hematite nanotube array to acetone, we measured responses to various gases such as ethanol, CO, H₂, CH₄, NH₃, C₇H₈, and C₆H₆ at 350 °C as shown in Figure 3b. Evidently, the hematite nanotube array displays the highest sensitivity to acetone. Fe₂O₃ is known to accelerate the oxidation (or combustion) of gases containing methyl groups such as acetone (methyl–methyl ketone), methanol (methyl alcohol) and butatone (methyl–ethyl ketone) at elevated temperatures under oxidizing atmosphere.^{31,32} The large surface area of the hematite nanotube array promotes the reported oxidation of acetone. Thus, the hematite nanotubes themselves has been used as catalysts to oxidize acetone to the final products, CO₂ and H₂O. Therefor the excellent sensitivity for acetone can be attributed to the catalytic role of hematite nanotube to promote the oxidation of methyl groups. For comparison, Figure 3c presents a bar graph of the responses of dense planar hematite films and hematite nanotube array toward eight interference gases at a concentration of 50 ppm. Compared to reference dense planar hematite films, the hematite nanotube array shows higher response to various gases. We can clearly identify that the hematite nanotube array showed the highest sensitivity and selectivity toward acetone gas as opposed to any other gas. To find the optimal sensing temperatures for acetone and ethanol gases, responses of the hematite nanotube array to 50 ppm acetone and ethanol were measured at temperatures ranging from 300 to 450 °C, as shown in Figure 4a. First of all, the hematite nanotube array shows highest response to acetone at 350 °C. The response ratio, $S_{\text{acetone}}/S_{\text{ethanol}}$, is higher than 2.1. Not only supreme sensitivity, the hematite nanotube array also exhibits extremely high selectivity to acetone at the temperature. As shown in Figure 4b, the 90% response time of the

hematite nanotube array is about 3 s, which is much shorter than that of the dense-planar hematite film (28 s, see the Supporting Information, Figure S4). To evaluate the detection limits of the hematite nanotube array to acetone, we measured the response curves of the hematite nanotube array to 1–5 ppm acetone at 350 °C. The responses of the hematite nanotube array are 10.28, 13.21, 15.6, 17.7, and 20.1 to 1, 2, 3, 4, and 5 ppm acetone. Although the 0.5 ppm concentration was the lowest experimentally examined in the present study, the theoretical detection limit (signal-to-noise ratio >3)³³ is calculated to be approximately 1.71 ppb for acetone (Figure 4c, see the Supporting Information for details). Detection limits of subppb levels to acetone demonstrate the potential of the sensor for use in high performance acetone sensors. Because acetone is found in the breath of patients with diabetes mellitus (acetone 0.1–10 ppm),¹⁵ we suggest that the hematite nanotube array synthesized by anodization is very promising for use in high-quality sensor materials for breath analyzers to diagnose diabetes mellitus. Figure 4d shows the change of response of the hematite nanotube array to 50 ppm acetone for 48 days. During the test, the hematite nanotube array repeatedly recovered its original base resistance. Furthermore, the hematite nanotube array could be subjected to long-term operation without degradation.

In summary, we have developed an effective and viable anodization method to obtain highly ordered and uniform hematite nanotube array for sensor application. Using the method, a vertically ordered hematite nanotube array could be directly synthesized on patterned Si substrates and then used for gas sensors without additional process. Our hematite nanotube array displayed ultrahigh and selective responses to acetone with detection limits down to a few parts per billion and response time shorter than 3 s. Excellent selectivity and ppb-level detection limits toward acetone demonstrate the promising potential of the hematite nanotubes for breath

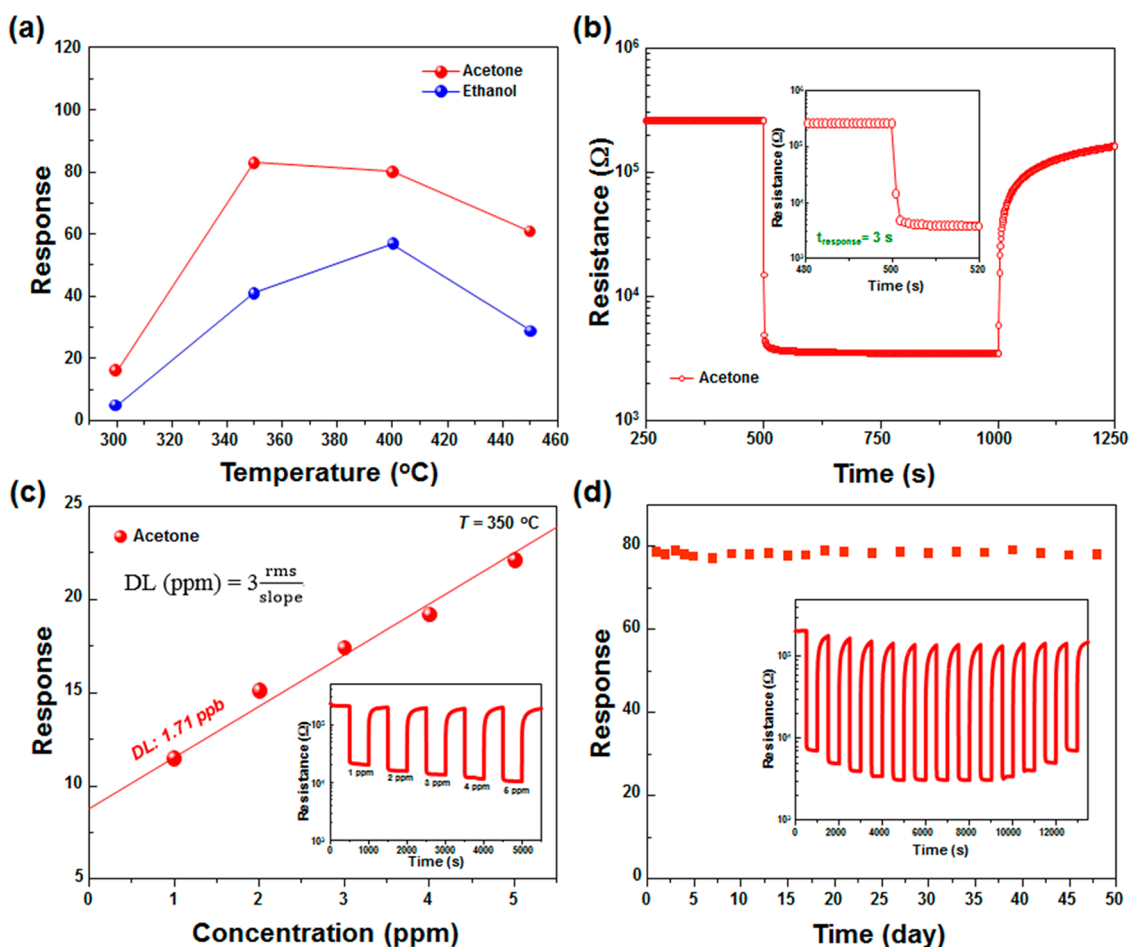


Figure 4. (a) Responses of the hematite nanotube array to 50 ppm acetone and ethanol as a function of temperature. (b) Dynamic acetone sensing transient of hematite nanotube array at 350 °C. Inset: 90% response time (t_{response}) of the hematite nanotube array. (c) Theoretical detection limits (DL) of hematite nanotube array to acetone. Inset: response curve of the hematite nanotube array to 1–5 ppm acetone at 350 °C. (d) Change of response of hematite nanotube array to 50 ppm acetone for 48 days. Inset: response to 13 consecutive pulses of 10–50 ppm acetone after 48 days of operation.

analysers to diagnose diabetes mellitus. Furthermore, highly aligned hematite nanotube array with high surface area to volume ratio can open new energy and environment applications including solar cells, water splitting cells, batteries, CO₂ conversion cells, and water purification membranes.

■ ASSOCIATED CONTENT

📄 Supporting Information

Detailed information about the sensor fabrication, characterization, sensor measurements, calculation of theoretical detection limits, morphologies and 90% response time of the hematite nanotube array and the dense-planar hematite film, and the gas sensing mechanism of the hematite nanotube array sensor. This material is available free of charge via the Internet at <http://pubs.acs.org>.

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Notes

The authors declare no competing financial interest.

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